



# Monitoring and tracking satellites and space debris using the electro-optical system

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# TYPES OF SATELLITE ORBITS

- Orbit height

- Low Earth Orbit (LEO)

- Altitude 360-2,000km
    - Satellite speed ~ 8km/sec
    - Orbital period ~ 90 min
    - Example: Globstar, 48 satellites in six planes, 1413km

- Medium Earth Orbit (MEO)

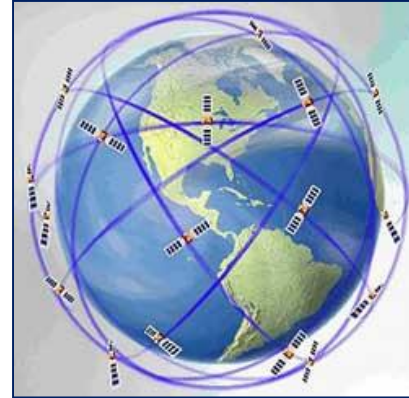
- Altitude 2,000km -35,786km
    - Satellite speed 8km/sec to 3 km/sec
    - Orbital period 2 to 24h
    - Example: GPS, 24 satellites in 6 planes, 20,200km

- Geosynchronous orbit (GSO)

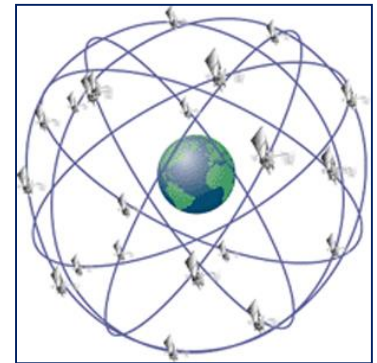
- Altitude 35,768km
    - Satellite speed ~ 3km/sec
    - Non zero inclination
    - Orbital period 24 hours

- Geostationary orbit (GEO)

- GSO satellite in zero inclination orbit

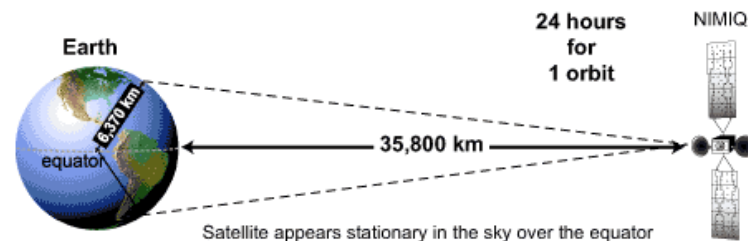


Constellation of Globstar system



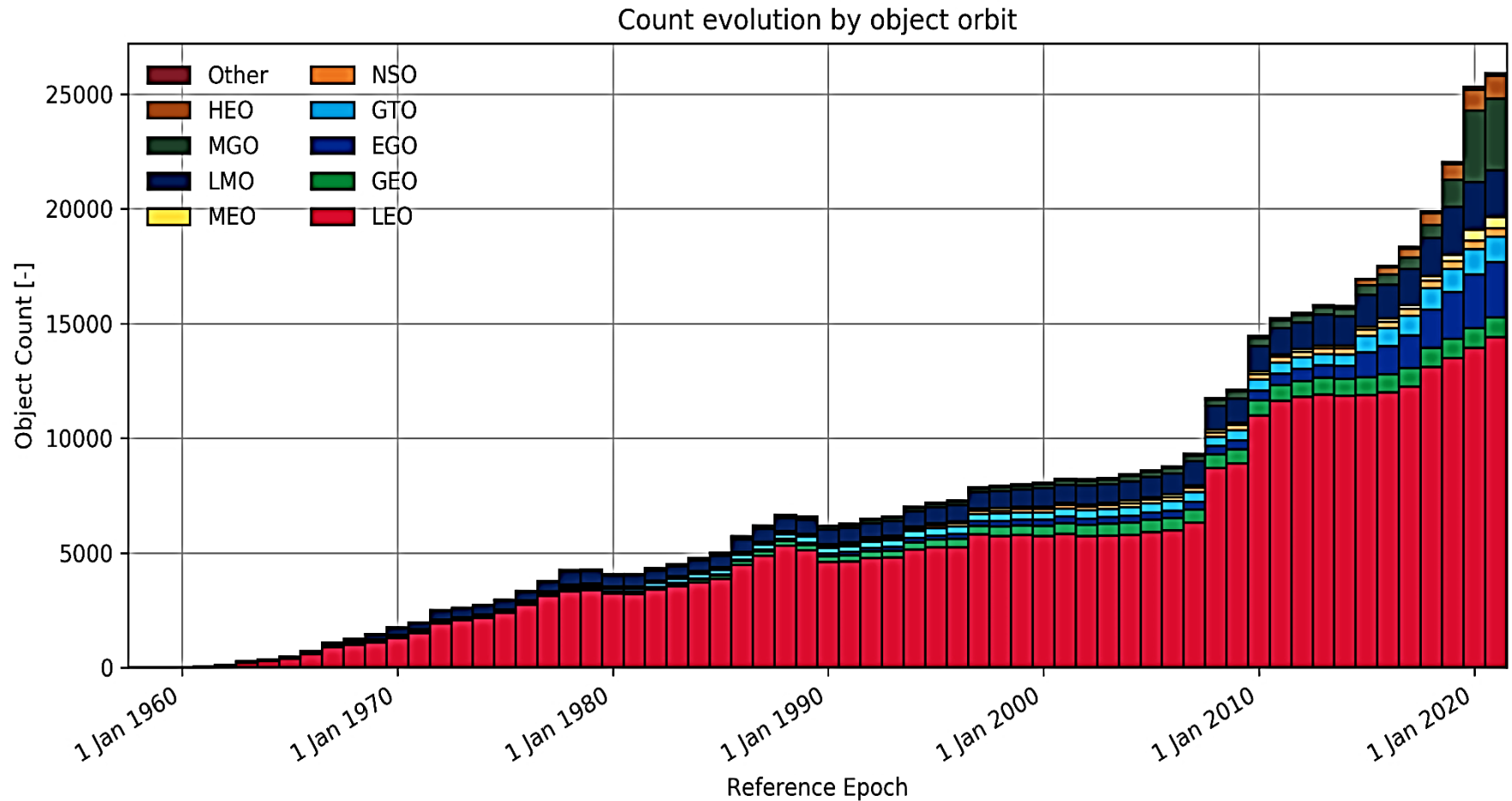
Constellation of GPS system

## Geostationary Orbit



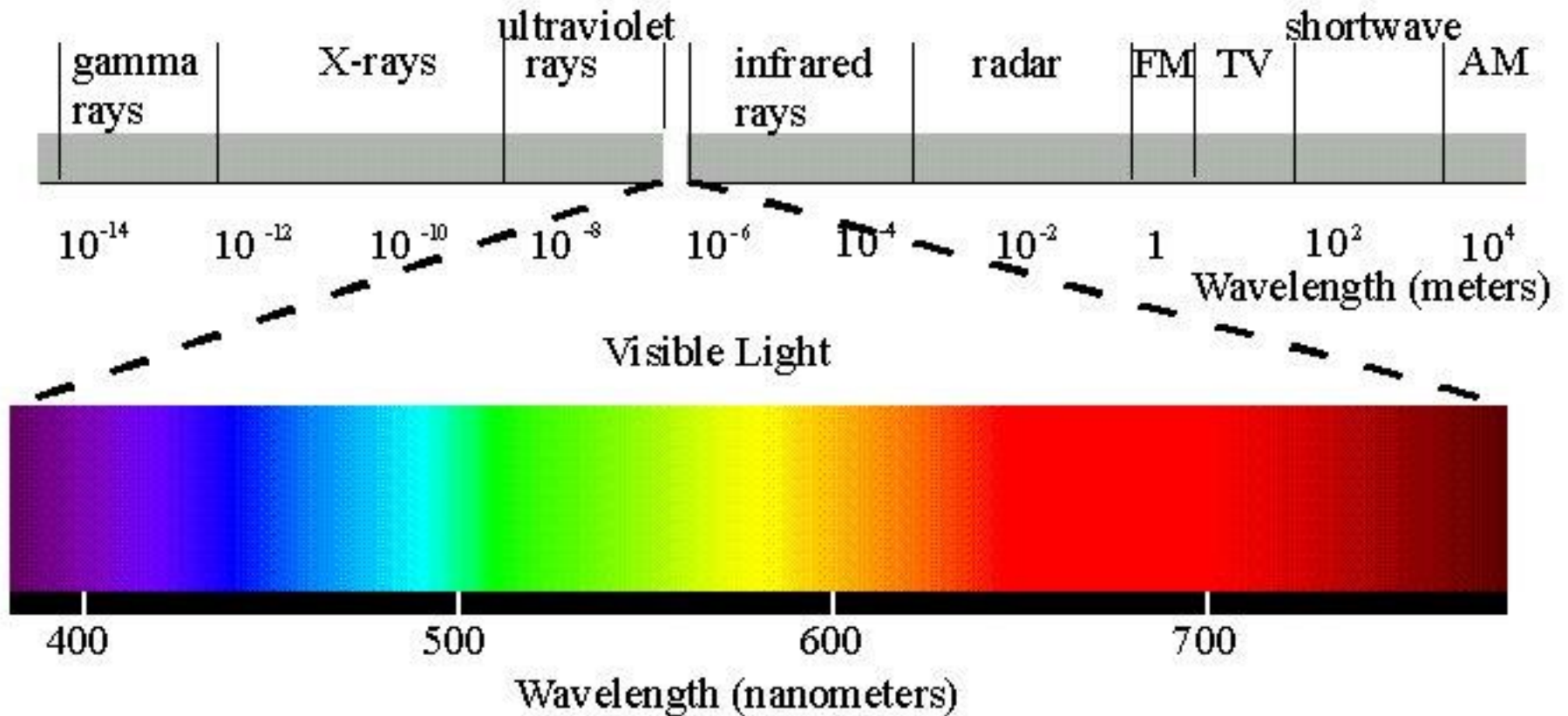


# Count Objects in Orbit



<https://sdup.esoc.esa.int/discosweb/statistics/>

# Electromagnetic Spectrum






## Ground based optical observations:

### ❑ active systems (send – receive)

- Radar observation.
- Laser observation.



Suitable for LEO  
Orbits

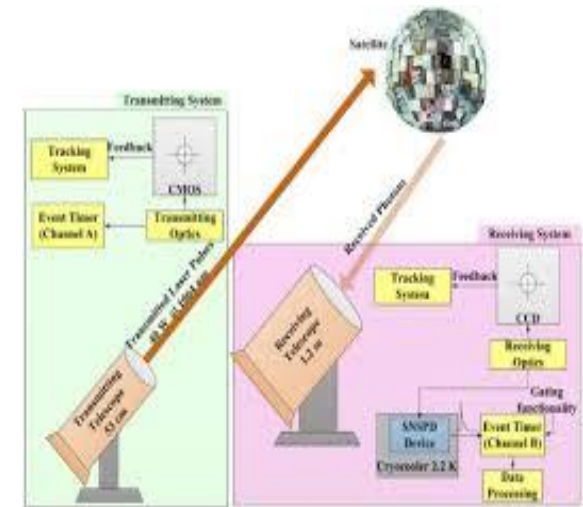
### ❑ passive systems (receive)

- Photographic observation (electro-optics).
  - 1- Telescope
  - 2- CCD camera

- Photographic observation generates respective (angle) information. Radar and laser observation generates information such as the distance (range), distance change (range rate), and angle with respect to the observer.

## ACTIVE SYSTEMS

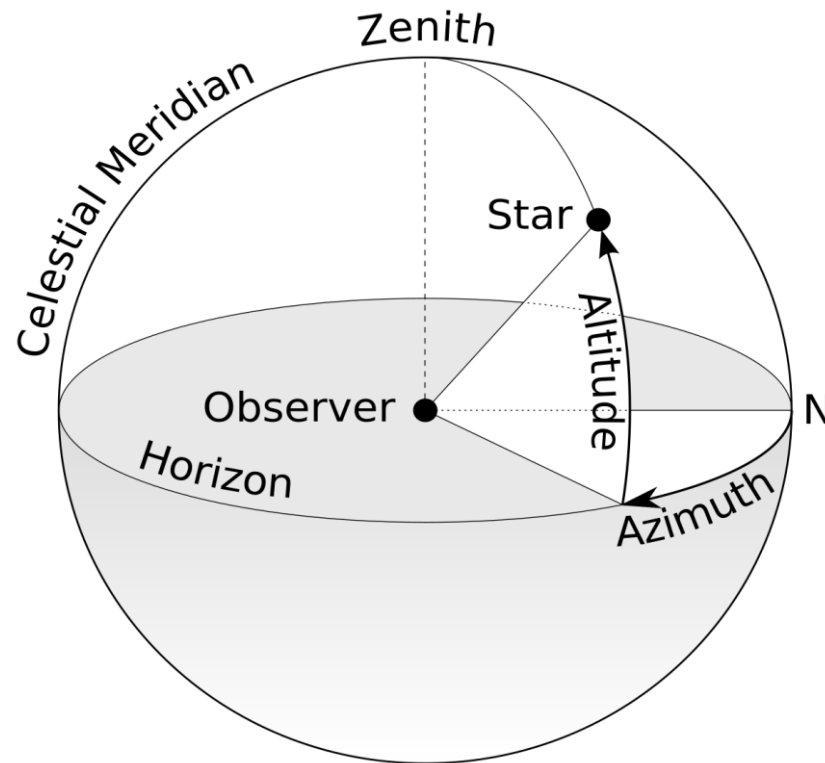
- Laser systems
  - very small area on the sky.
  - Very sharp pulse
- Radar systems
  - Low resolving power.
  - Very high pulse power.



## The horizontal coordinate (Alt-Az):

The **horizontal** coordinate system is based around an observers (or telescopes)  $360^\circ$  field of view, and the position of a target is given with respect to the observers local horizon. The system is fixed to the Earth and not the stars, with coordinates determined as follows:

- The **altitude** is the [angle](#) between the object and the closest point on the observer's local horizon (green curve in image). It can take any value between  $0^\circ$  and  $90^\circ$ .
- The **azimuth** (Az) is the angle of the object around the horizon, running from the north point towards the east (red curve in image). It can take any value between  $0^\circ$  and  $360^\circ$ .

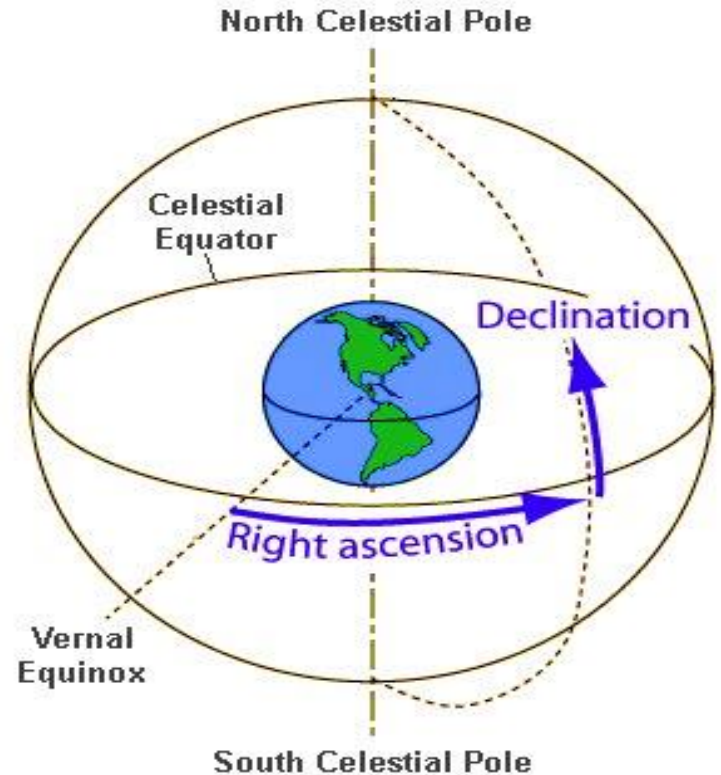


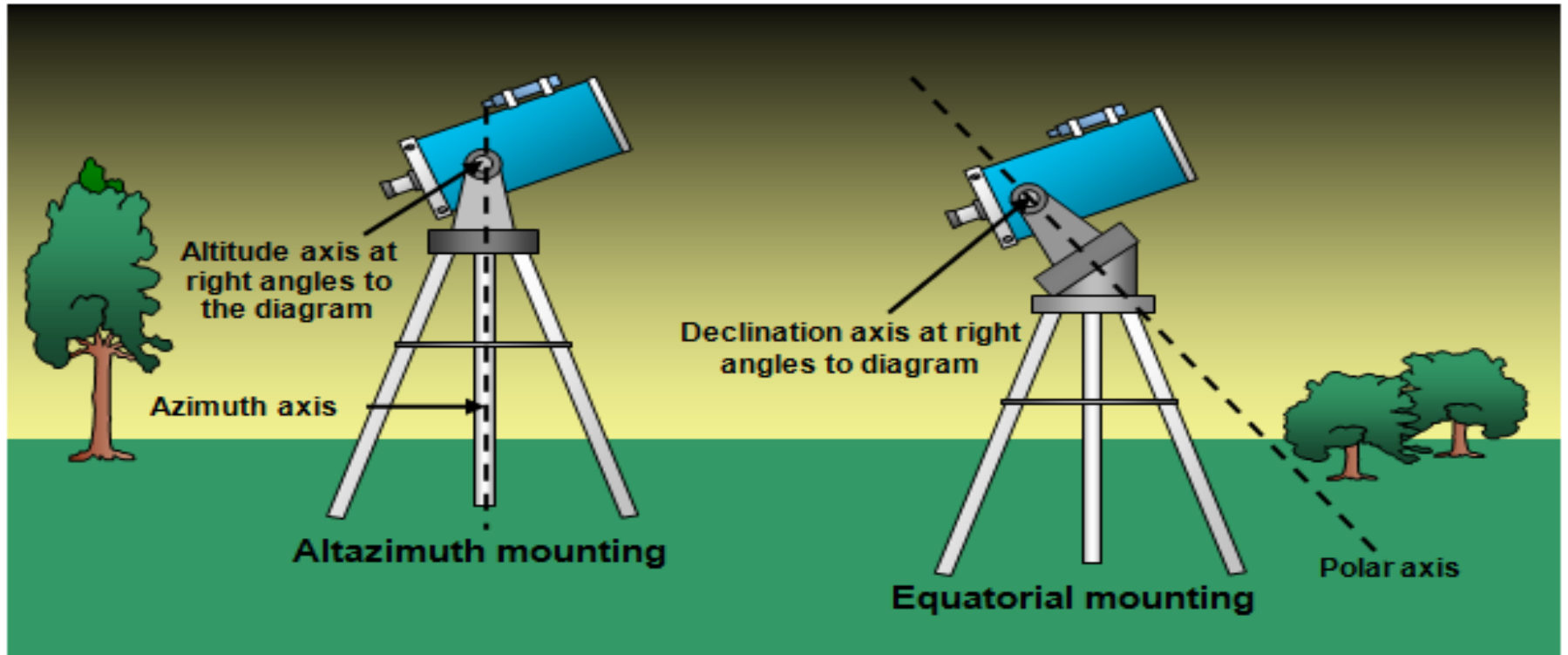


## 1- Equatorial Coordinate:

The **equatorial** coordinate system allows observers (or telescopes) to locate celestial objects using coordinates that are fixed in relation to the stars. The equatorial coordinates are then determined as follows:

- The **Declination** (Dec) measures the angle of an object above or below the celestial equator. It can take any value between  $-90^\circ$  and  $90^\circ$ .
- The **Right Ascension** (RA) measures the angle of the arc that runs from the vernal equinox, along the celestial equator, to the closest point to the object. Unlike other systems, the RA is measured in hours instead of degrees, and can take any value between 0 and 24 hours. Note that there are  $(360/24) = 15^\circ$  in one hour of right ascension.





# Why photo-graphic?

	<b>Electro-optics</b>	<b>Radar</b>	<b>Laser</b>
Detection of satellites	Yes	Yes	No
Following the track of satellites	Yes	Yes	Yes
Photometric observations of satellites	Yes	No	No
Physical parameters of satellites	Yes	No	No
Type detection of satellites	Yes	No	No

# Satellite visibility

In order to observe a satellite in visible light, three conditions must be fulfilled:

1. The satellite must be above the horizon.
  2. The satellite must be illuminated by the Sun, i.e., it must not be in the Earth shadow.
  3. The station must be in the Earth shadow (Sun below  $-12^\circ$  elevation).
- LEO (Low Earth Orbit) satellites must with highest relative speed in the point of highest elevation. Usually they are also at brightest there. High speed leads to a long trail in the image, even the satellite is brighter. When the satellite becomes slower it usually becomes fainter also.
  - Due to the condition of being illuminated by the Sun a LEO satellite is best visible in the evening and/or in the morning hours. The time interval depends on the satellite's altitude and on the geographical latitude of the observation site. For the Egyptian sites, the time interval in evening and morning is about 60 to 120 minutes (seasonal differences).
  - The observation of MEO (Medium Earth Orbit, e.g., GPS satellite orbits) and GEO (Geostationary Earth Orbit) satellites are also possible to observe. Ideally, they are even illuminated most of the time.

## How we can choose system ?

- GEO survey. telescopes having FOV from 3.5 – 8 degrees
- Local (deep) GEO survey. telescopes having FOV 2–2.2 degree
- Tracking of bright (brighter than apparent magnitude of 15.5) GEO and HEO objects. telescopes of 25 cm aperture.
- Tracking of the faint (fainter than apparent magnitude of 15.5) space debris at GEO and GTO with 40–80 cm aperture telescopes.
- Tracking observations of LEO objects with 12.5–25 cm aperture telescopes and survey of HEO objects with 18-cm telescope can be adjusted.

## Field of view calculation

$$FOV[^\circ] = 2 * \arctan\left(\frac{p * I}{2 * F}\right) * \frac{180}{\pi} = 2 * \arctan\left(\frac{S}{2 * F}\right) * \frac{180}{\pi}$$

$$FOV_{pixel}["] = 2 * \arctan\left(\frac{p * I}{2 * F}\right) * \frac{180}{\pi} * \frac{3600}{I} \approx \frac{p}{F} * \frac{180}{\pi} * 3600$$

with:  $FOV_{pixel}$  = FOV of each pixel, given in arc-seconds

$FOV$  = field of view in degree

$p$  = pixel size, mm per pixel

$I$  = image size in pixels

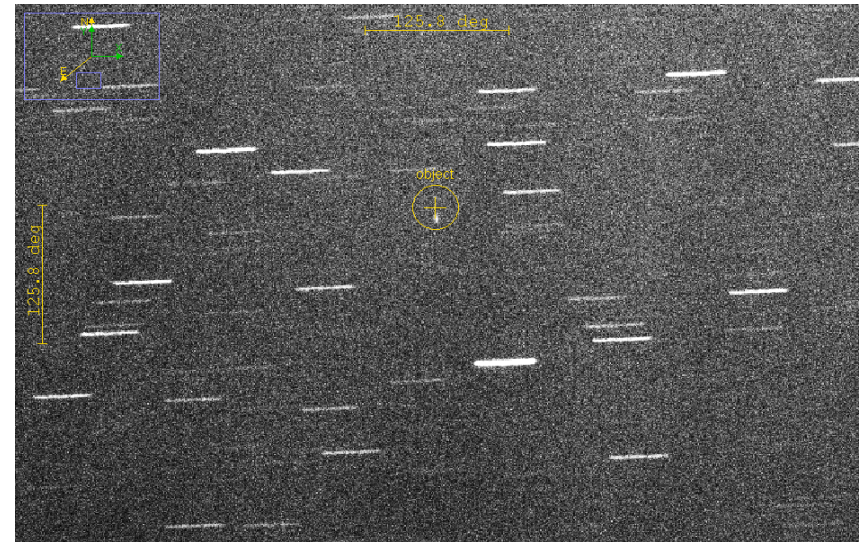
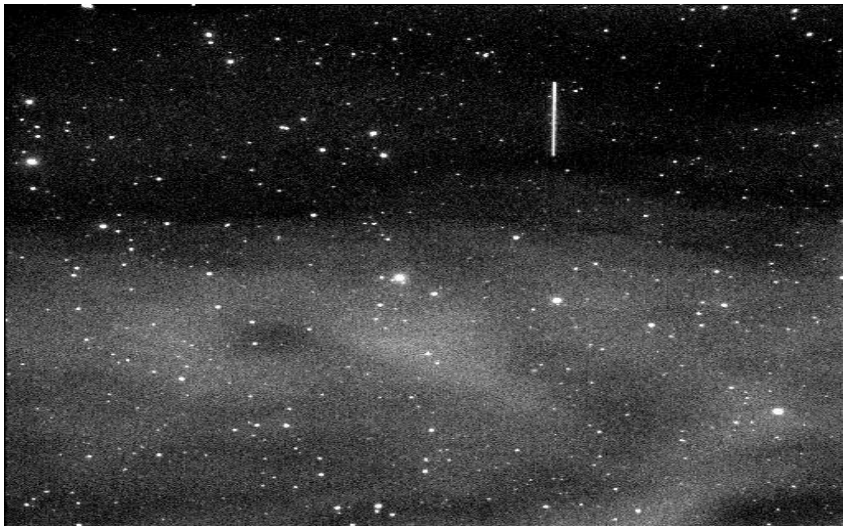
$F$  = focal length in mm

$S$  = used sensor length in mm

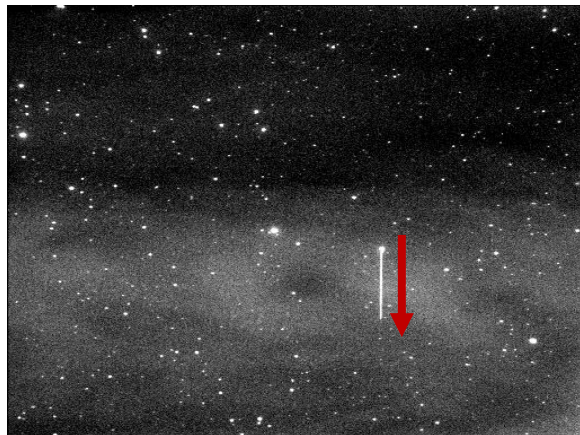
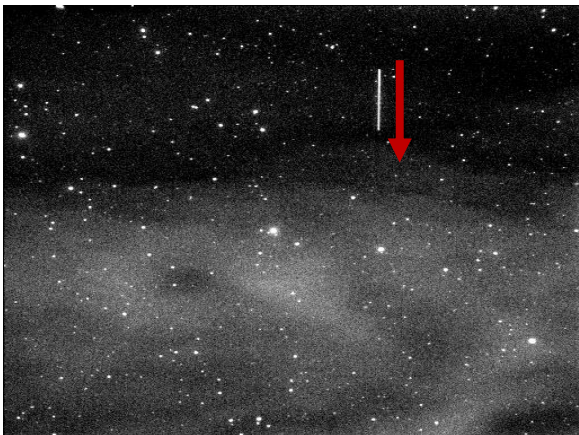
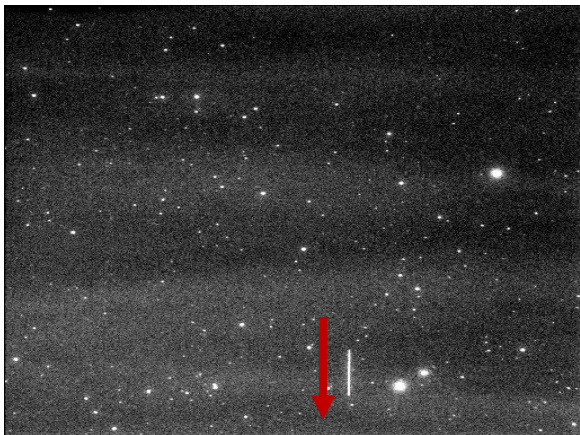
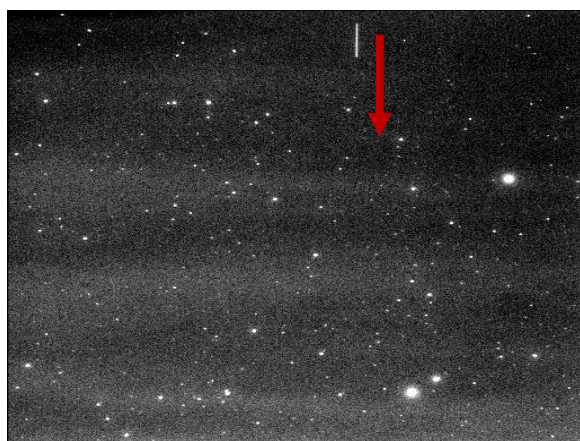
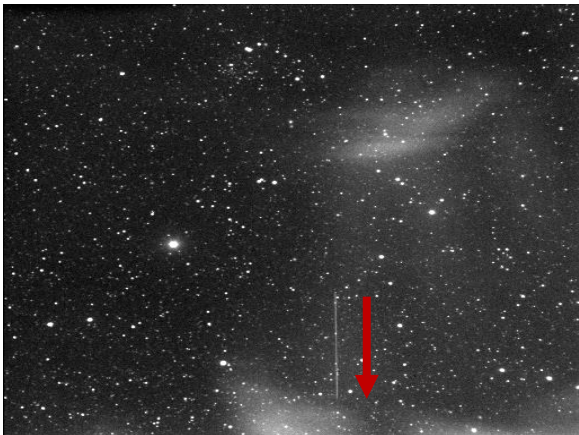
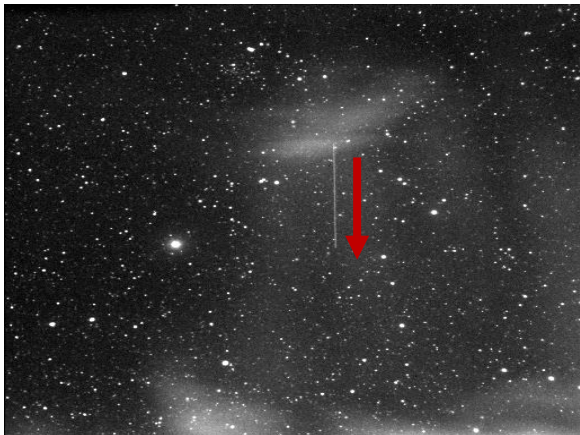


# Known objects tracking techniques

- Leap frog tracking: the stars appear as points while the tracked object produces an arc, whose length is determined by the angular velocity of the object and the exposure time
- Continuous Tracking: Images taken in this mode show the object as small point and the stars as arcs





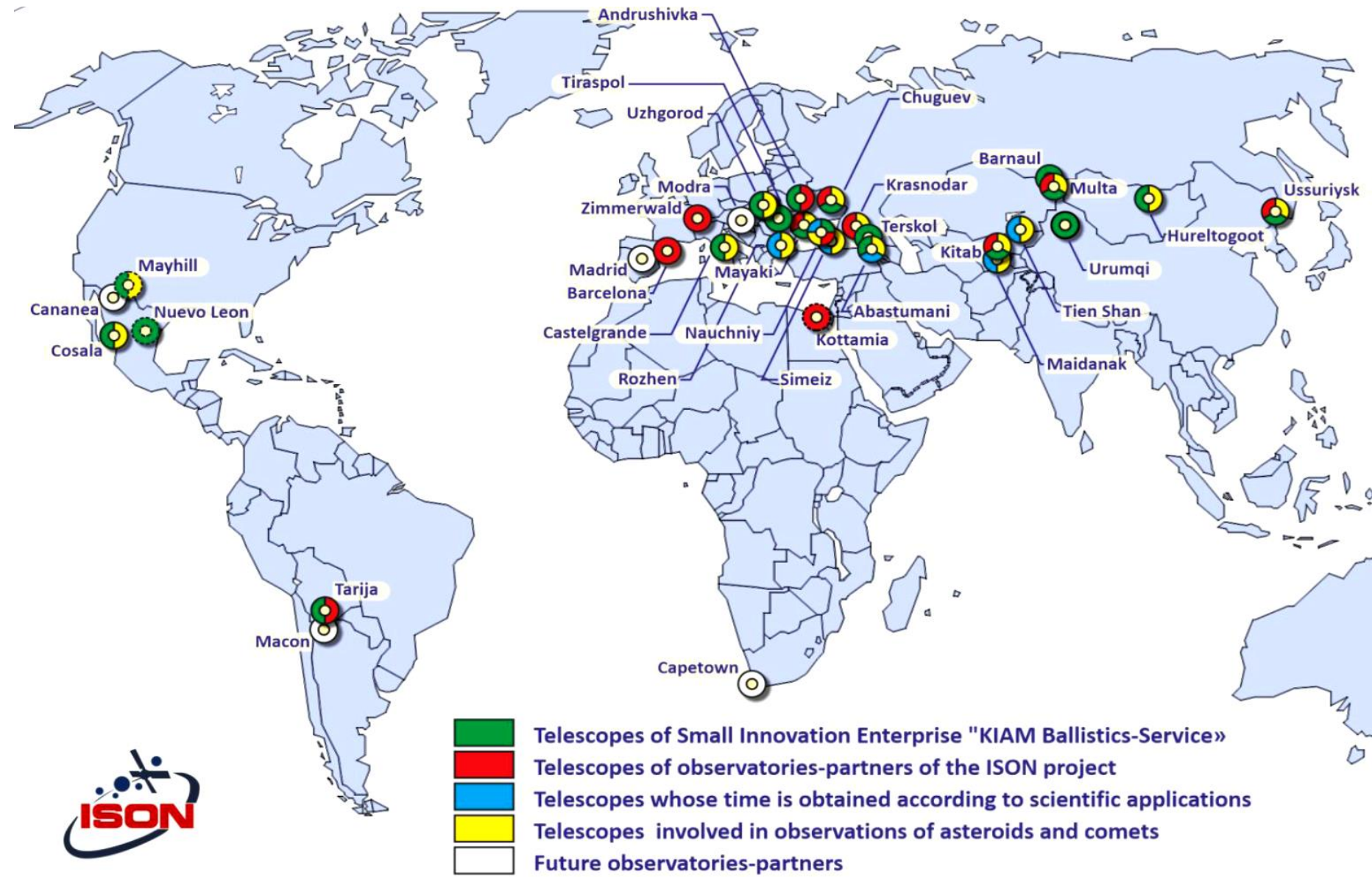


# Unknown objects observations

1. Detection: Activities to detect incoming satellites and space debris, projectiles, space objects within the observed angles of the monitoring facilities.
2. Tracking: Activities to track the object within the initial orbit of 'detection.
3. Calculation: Activities to determine orbits
4. Identification: Activities to identify the mission and nationality of the detected object with the precise orbit elements through 'detection' and 'tracking'.
5. Cataloging: Activities to manage the database of collected data such as name, identification number, orbit elements, mission, etc.
6. Assessments: Activities to calculate the close approaches between two objects satellites and /or debris to analyze the conjunction and collision probability with dangers debris



# International Scientific Optical Network (ISON)



# system structure

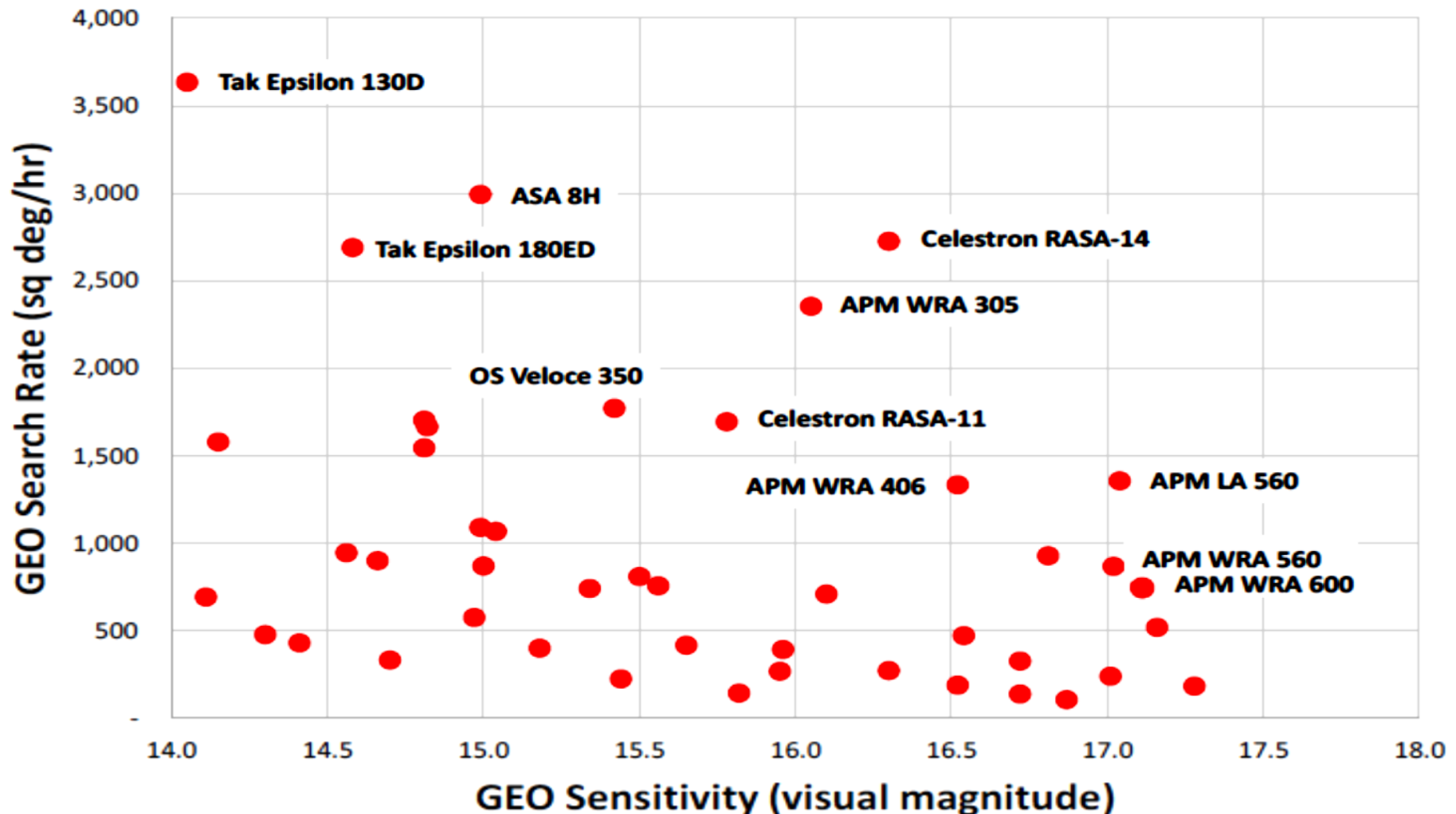
## Hardware :

- Mount
- Tube
- CCD Camera
- GPS unit

## Software :

- Mount control
- Camera control
- Image analysis
- orbit determination

# COTS Astrograph Sensitivity VS Search Rate



\*Ackermann, M., Zimmer, P., McGraw, J., & Kopit, E. (2015). COTS Options for Low-Cost SSA. In Proceedings of the Advanced Maui Optical and Space Surveillance Technologies Conference. Maui, Hawaii.



# Optical Satellite Tracking Station (OSTS)-NRIAG

Items	Characteristics
Telescope Series	Celestron 11" Rowe-Ackermann Schmidt Astrograph with CGE Pro Mount
Telescope Aperture	11"
Telescope Focal Ratio	f/2.2
Telescope Focal Length	620 (mm)
Focuser Style	Internal Moving Primary
Focuser Speed	Dual Speed
Telescope Mount Type	Equatorial
CCD device	FLI MicroLine ML11002 Monochrome Camera Grade 2
Pixels	4072 x 2720 pixels
Pixel Size (μm)	9.0 x 9.0
Cooling	Peltier 55°C below ambient Temperature
Interface	USB 2.0
System (FOV)	3.4°×2.3°



# Telescope control software

CHAOS TCS 2.3.4 (Automatic Mode) - Observer


File Operation Imaging Tracking Dome Commands Settings

#	Exp	T	Target	$\alpha$	$\delta$	$\dot{\alpha}$ ["/min]	$\dot{\delta}$ ["/min]	$\Delta\alpha'$	$\Delta\delta'$	$m$	Exposure [s]	Filter
178		HA	dummy_090229	07 <sup>h</sup> 41 <sup>m</sup> 47 <sup>s</sup> .95	+32° 24' 30".4					15.4	0.1	
179	10	HA	090229005007	07 <sup>h</sup> 41 <sup>m</sup> 41 <sup>s</sup> .87	+32° 24' 30".4					15.4	10 x 20	
180		HA	dummy_070005	02 <sup>h</sup> 59 <sup>m</sup> 00 <sup>s</sup> .44	+12° 22' 53".1					15.0	0.1	
181		HA	070005008000	02 <sup>h</sup> 56 <sup>m</sup> 40 <sup>s</sup> .95	+12° 22' 53".1					15.0	10 x 8.5	
182		HA	dummy_090089	03 <sup>h</sup> 25 <sup>m</sup> 51 <sup>s</sup> .04	+10° 07' 48".6					15.7	0.1	
183	10	HA	090089002007	03 <sup>h</sup> 31 <sup>m</sup> 37 <sup>s</sup> .95	+10° 07' 48".6					15.7	10 x 20	
184		HA	dummy_098701	05 <sup>h</sup> 39 <sup>m</sup> 41 <sup>s</sup> .65	+10° 35' 12".5					14.0	0.1	
185		HA	098701003009	05 <sup>h</sup> 41 <sup>m</sup> 50 <sup>s</sup> .15	+10° 35' 12".5					14.0	10 x 19.5	
186		HA	dummy_094096	05 <sup>h</sup> 33 <sup>m</sup> 36 <sup>s</sup> .89	+12° 41' 41".2					14.5	0.1	
187	8	HA	094096002009	05 <sup>h</sup> 33 <sup>m</sup> 50 <sup>s</sup> .63	+12° 41' 41".2					14.5	10 x 20	

Control

Observer

Mode: **Automatic**

**Running** 

Imaging

Camera: **EXPOSURE**

Exposure: 10 x 20 s

Prefix:

Interv: s #: 3526

Frame: **Full**

Target Correct

Name: 094096002009

$\alpha$ : 05<sup>h</sup> 33<sup>m</sup> 36.43<sup>s</sup>

$\delta$ : +12° 41' 41.2"

$t$ : 22<sup>h</sup> 39<sup>m</sup> 50.30<sup>s</sup>

Pointing: **Idle**

Tracking

Sidereal: **OFF**

$t$ : 8.51408 "/s

$\delta$ : 1.22971 "/s **ON**

Filter:

Observation conditions

Temperature: +10 °C Humidity: 50 %

Air pressure: 1013.2 hPa

Sun

$\alpha$  = 16<sup>h</sup> 39<sup>m</sup> 26.84<sup>s</sup>

$\delta$  = -22° 08' 46.4"

$t$  = 11<sup>h</sup> 35<sup>m</sup> 05.96<sup>s</sup>

$A$  = -37° 05' 56.2"

$h$  = -80° 24' 54.6"

Moon

$\alpha$  = 22<sup>h</sup> 44<sup>m</sup> 55.84<sup>s</sup>

$\delta$  = -13° 28' 39.9"

$t$  = 05<sup>h</sup> 29<sup>m</sup> 36.96<sup>s</sup>

$A$  = -105° 26' 01.7"

$z$  = 90° 16' 52.7"

Tube position (obs.)

$\alpha$  = 05<sup>h</sup> 31<sup>m</sup> 08.10<sup>s</sup>

$\delta$  = +12° 34' 35.4"

$t$  = 22<sup>h</sup> 43<sup>m</sup> 24.71<sup>s</sup>

$A$  = +130° 17' 33.8"

$z$  = 24° 48' 55.6"

Time

Date: **2019-12-03**

UTC: **21:17:38.4**

LST: **04 14 33.7**

# Camera control software

CameraControl 3.8 - [E:\Images\2019\12\03\098019004002.20191203.200138.fit]

File Camera Tools Help

Target description  
Object: 098019004002  
t: 22h 19m 50.94s  
δ: -08° 09' 38.9"  
Filter: ☐ None

Orientation  
☐ 0°  
☐ 90°  
☒ 180°  
☐ 270°  
☐ Mirror

Grab Drift scan

Exposure: 12.5 s **Stop !**  
Image size: Custom ☐ Video  
☐ Auto save: 36830.20191118.172546

Dark Frame  
☐ None ☒ Also ☐ Only  
☐ Reuse Dark Frame **Upload ...**  
☐ Use Dark Frame Library

☐ Sequence  
Frames: 200 Interval: s

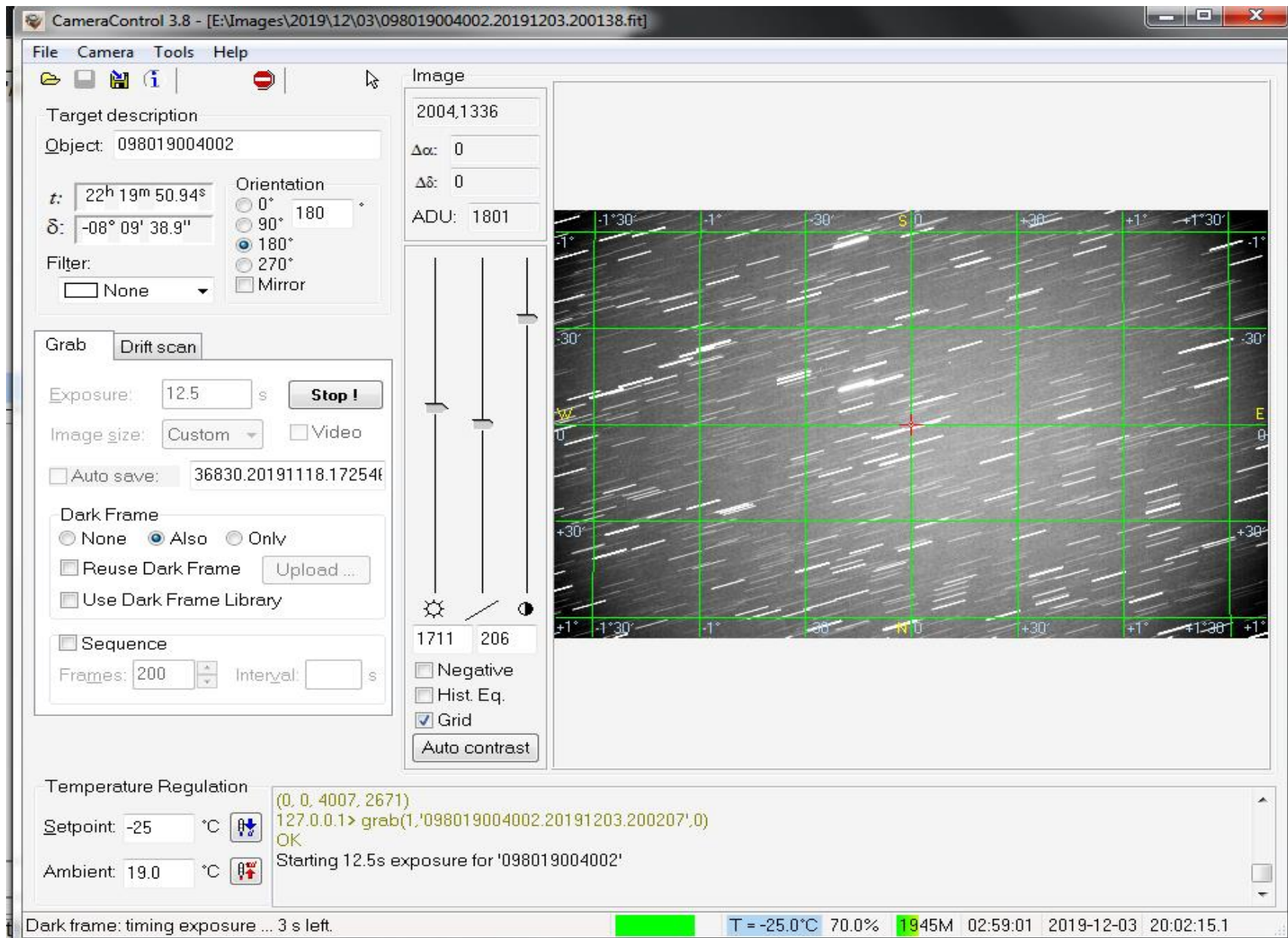
Image  
2004,1336  
Δα: 0  
Δδ: 0  
ADU: 1801

1711 206  
☐ Negative  
☐ Hist. Eq.  
☒ Grid  
**Auto contrast**

Temperature Regulation  
Setpoint: -25 °C  
Ambient: 19.0 °C

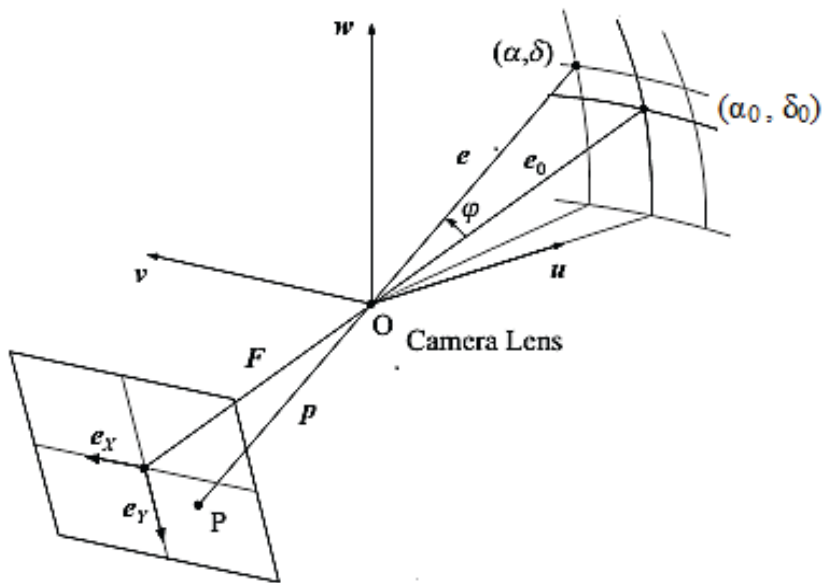
(0, 0, 4007, 2671)  
127.0.0.1> grab(1,'098019004002.20191203.200207',0)  
OK  
Starting 12.5s exposure for '098019004002'

Dark frame: timing exposure ... 3 s left. T = -25.0°C 70.0% 1945M 02:59:01 2019-12-03 20:02:15.1



## ASTROMETRY PROCESSING

Astrometry is the science of measuring the positions of celestial objects. In CCD images, the first step is to determine the centroids of a set of stars (called reference stars) with known spherical coordinates, and also the centroids of the images of the objects whose position you wish to measure (that is, the target stars)



$$\alpha = \alpha_0 + \arctan \frac{-X}{\cos(\delta_0) - XY \sin(\delta_0)}$$

$$\delta = \arcsin \frac{\sin(\delta_0) - Y \cos(\delta_0)}{\sqrt{1 + X^2 + Y^2}}$$

# Sample image processing using background field stars

Random image of OSCAR-11

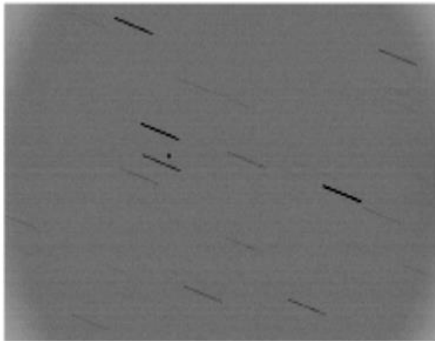
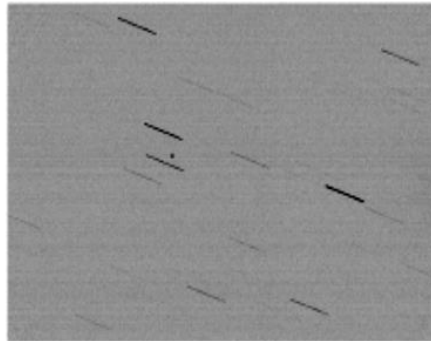
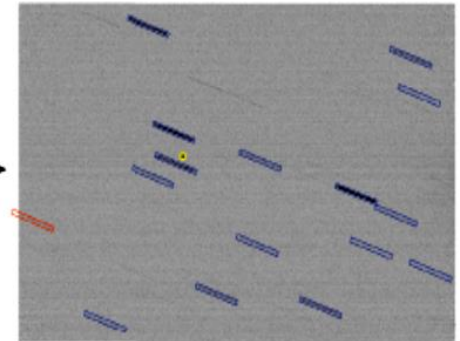


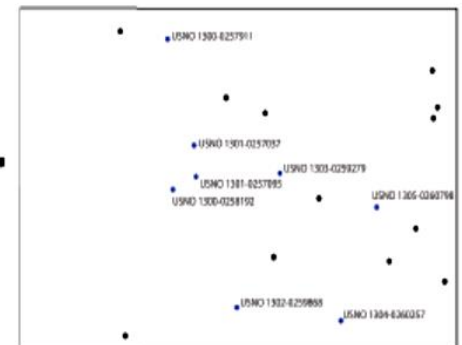
Image preprocess



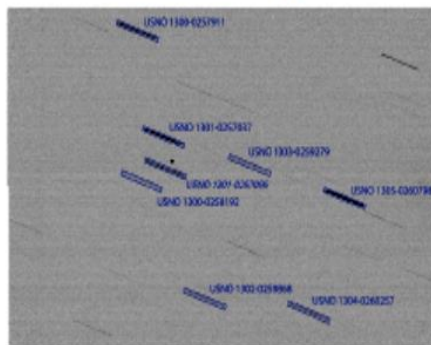
Star streak detection



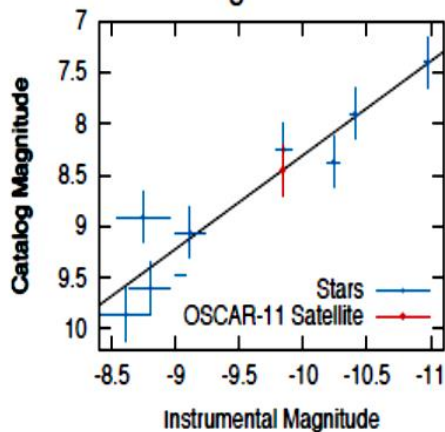
Star identification



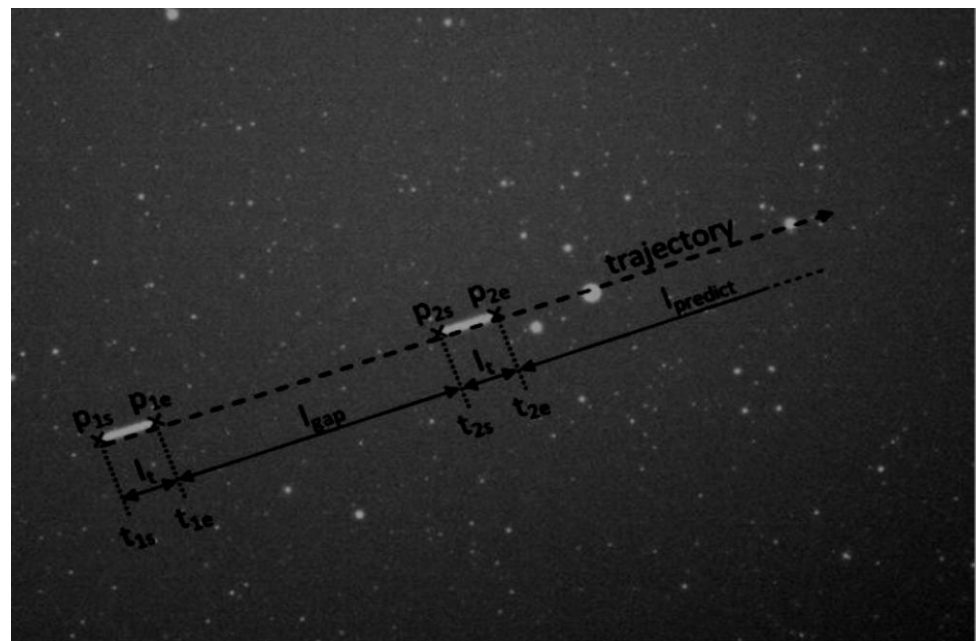
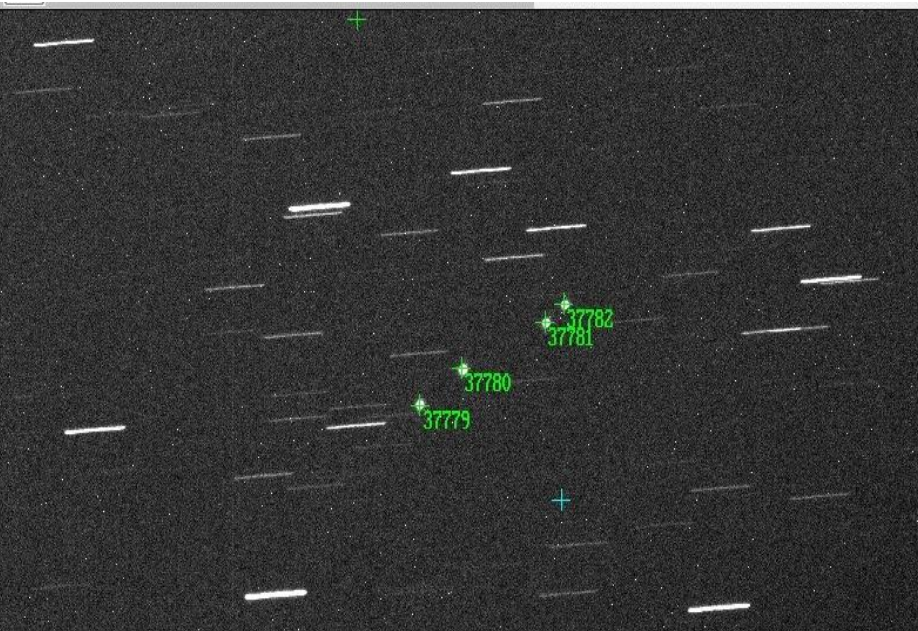
Photometry



Regression









# SW of Orbit determination

## Input data

- Measurements from optical system
- Current and forecasted geophysical data

## Modules

- Initial orbit determination
- Analytical module for quick estimation of propagation
- Precise orbit determination

## Subroutine required

- Coordinates transformation
- Earth gravitational potential
- Third body effect
- Atmospheric drag
- solar radiation pressure
- Least square technique and extended Kalman filter

## output data

- orbital elements
- Observation plan for optical system

Orbit determination is a method of determining state of a satellite as a function of time using angles-only observations. The orbit determination problem consists of two basic parts: obtain an initial orbit and refine the orbit derived from the initial orbit determination (IOD) method. angles-only methods are used for initial orbit determination and least squares technique is used to refine orbit.

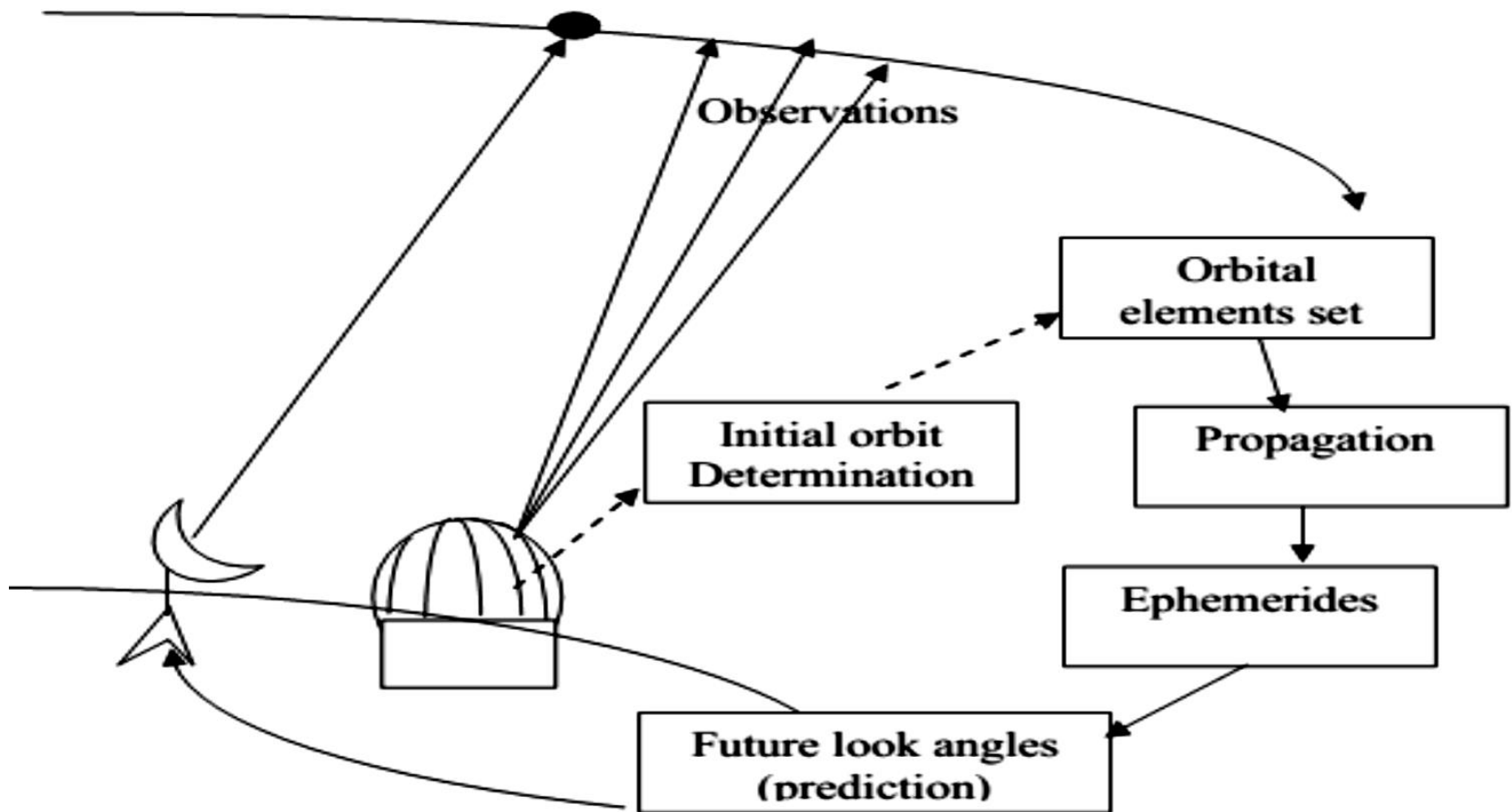
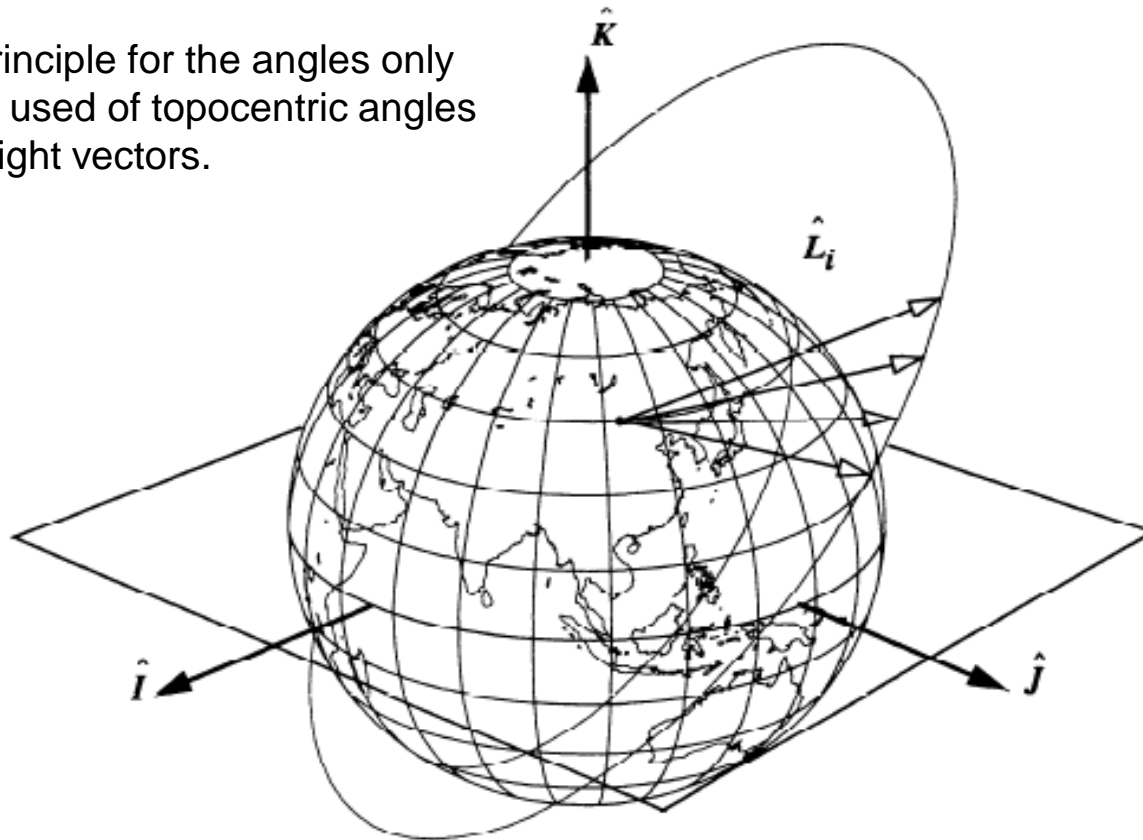


Figure shows principle for the angles only technique is the used of topocentric angles to form line-of-sight vectors.



Geometry of angles only observation

## ANGELS ONLY ORBIT DETERMINATION

$$\vec{r}_{site} = \begin{pmatrix} C \cos(\varphi_{gc}) \cos(\lambda_{gc}) \\ C \cos(\varphi_{gc}) \sin(\lambda_{gc}) \\ S \sin(\varphi_{gc}) \end{pmatrix}$$

$$C = \frac{R_E}{\sqrt{1 - e_E^2 \sin^2(\varphi_{gc})}} + H, \quad S = C (1 - e_E^2) + H$$

$$\hat{L} = \begin{pmatrix} \cos(\delta_t) \cos(\alpha_t) \\ \cos(\delta_t) \sin(\alpha_t) \\ \sin(\delta_t) \end{pmatrix}$$

$$\vec{r} = \rho \hat{q} + \vec{r}_{site}$$

# ANGELS ONLY ORBIT DETERMINATION METHODS

1. Gauss-Gibbs method.
2. Gauss H.Gibbs method.
3. Double R iteration.
4. Gooding method.

## GAUSS METHOD

The Gauss method begins with the first assumption that all three position vectors lie in a plane. There for, the following equation is valid for some unknown particular values of  $c_1$ ,  $c_2$ , and  $c_3$ .

$$c_1 \vec{r}_1 + c_2 \vec{r}_2 + c_3 \vec{r}_3 = 0$$

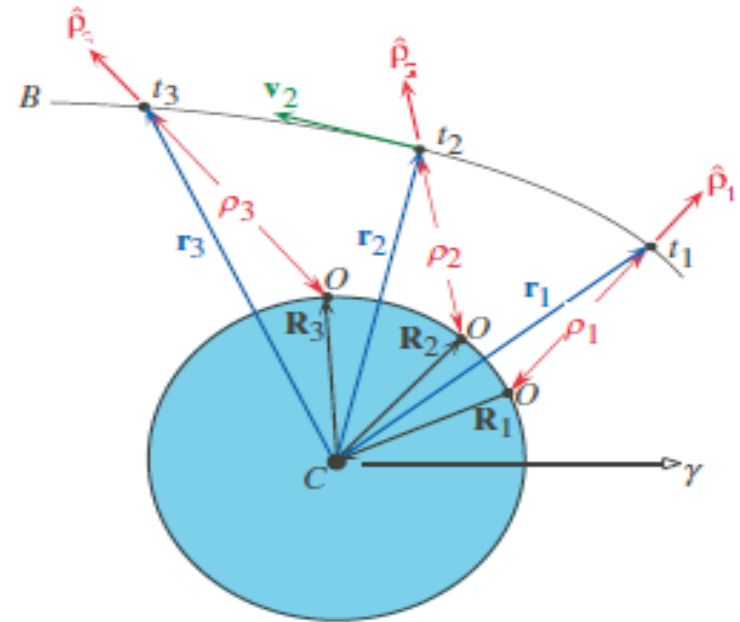
$$\vec{r}_1 \times \vec{r}_3(c_1) = \vec{r}_2 \times \vec{r}_3(-c_2)$$

$$\vec{r}_1 \times \vec{r}_3(c_3) = \vec{r}_1 \times \vec{r}_2(-c_2)$$

$$\vec{r}_1 \times \vec{r}_3(c_1) = \vec{r}_2 \times \vec{r}_3$$

$$\vec{r}_1 \times \vec{r}_3(c_3) = \vec{r}_1 \times \vec{r}_2$$

$$\vec{r}_i = f_i \vec{r}_2 + g_i \vec{V}_2 \quad , i = 1,3$$





# GIBBS METHOD

The Gibbs method uses three position vectors to determine the orbit. Solving Gibbs relies on knowing the Gauss formulation. The method works well for observations which have an angular separation greater than 1 degree.

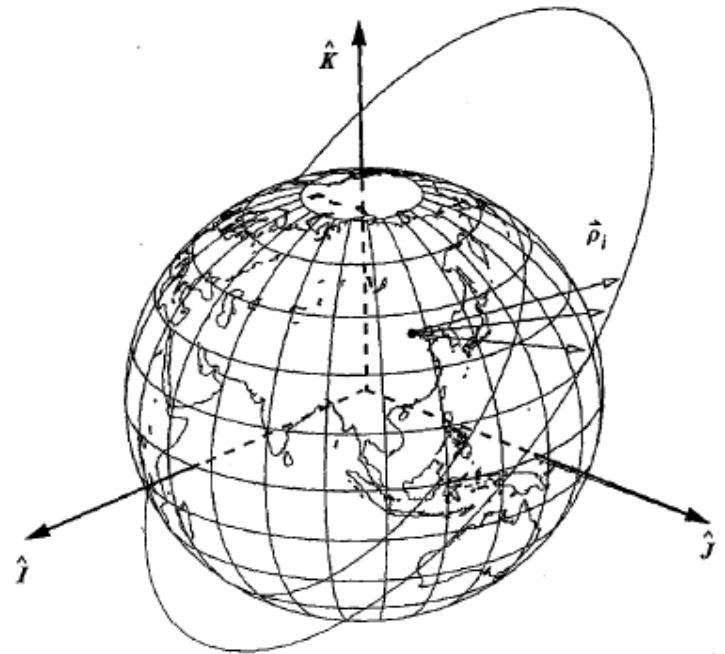
$$\vec{D} = \vec{r}_1 \times \vec{r}_2 + \vec{r}_2 \times \vec{r}_3 + \vec{r}_3 \times \vec{r}_1$$

$$\vec{N} = r_1(\vec{r}_2 \times \vec{r}_3) + r_2(\vec{r}_3 \times \vec{r}_1) + r_3(\vec{r}_1 \times \vec{r}_2)$$

$$\vec{B} = (r_2 - r_3)\vec{r}_1 + (r_3 - r_1)\vec{r}_2 + (r_1 - r_2)\vec{r}_3$$

Then, we will obtain the middle velocity vector

$$\vec{V}_2 = \frac{L_g}{r_2} \vec{U} + L_g \vec{B} \quad \text{Where } L_g = \sqrt{\frac{\mu}{ND}} \quad \text{and } \vec{U} = \vec{D} \times \vec{r}_2$$



# HERRICK -GIBBS METHOD

$$t_{12} = t_2 - t_1, t_{23} = t_3 - t_2, t_{13} = t_3 - t_1$$

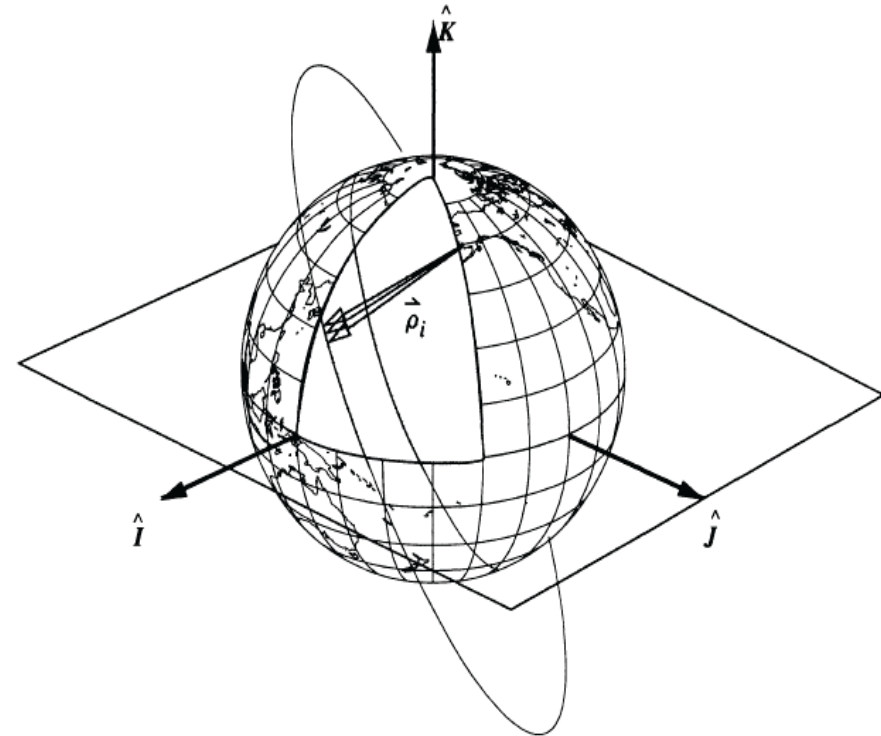
$$p_1 = \frac{t_{23}}{t_{12} t_{13}}, p_2 = \frac{t_{23} - t_{12}}{t_{12} t_{23}}, p_3 = \frac{t_{12}}{t_{23} t_{13}}$$

$$k_1 = \mu \frac{t_{23}}{12}, k_2 = \mu \frac{t_{23} - t_{12}}{12}, k_3 = \mu \frac{t_{12}}{12}$$

$$r_i = \sqrt{x_i^2}, \quad d_i = p_i + \frac{k_i}{r_i^3}, \quad i = 1, 2, 3$$

Finally, we will obtain the velocity vector

$$V_2 = -d_1 x_1 + d_2 x_2 + d_3 x_3$$



# DOUBLE R-ITERATION

In Double r-iteration technique, there are four main steps to arrive at a solution.

- 1) The first step bounds the guesses from the available information.
- 2) The second step, is the main idea of the technique Double r-iteration. The subsequent iterations use the second portion to determine intermediate guesses, so it is important to have a modular routine.
- 3) The third section begins the formal iterative process. It tries to align the times with the estimated values of the orbits.
- 4) Finally, a type of differential correction determines the answer.

## GOODING METHOD

Given values are  $\mathbf{R}_j$  ,  $t_j$  , and  $\hat{\rho}_j$  , for  $j = 1, 2, 3$

---

Assume a value for  $\rho_1$  and  $\rho_3$

---

**while** Not Maximum Iterations or Tolerance Reached *do*

---

Generate an estimated orbit by solving Lambert problem using  $\mathbf{r}_1$ ,  $\mathbf{r}_3$ , and  $t_3 - t_1$

---

Compute the error in the position measurement of the spacecraft at  $t_2$

---

Iterate  $\rho_1$  and  $\rho_3$  using the Newton-Raphson procedure

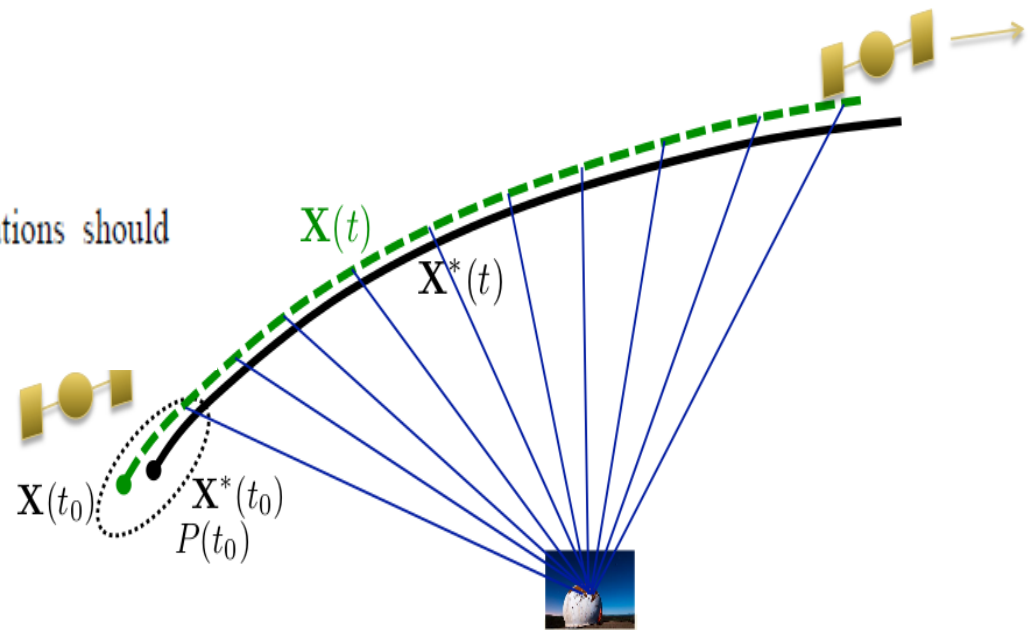
---

**end while**

---

# ORBIT DETERMINATION WITH DIFFERENTIAL CORRECTION

- 1- Pick an initial nominal state
- 2- Compute the values of the observed parameters  $Y_c$  at  $N$  times corresponding to the observations  $Y_o$ .
- 3- Compute the residuals or (O-C).
- 4- Calculate the partial derivatives.
- 5- Form the normal equations and solve it.
- 6- Update the elements
- 7- Lastly, apply the RMS test to determine if iterations should continue.





Thanks